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# Microwave cavity perturbation studies on H-form and ion-exchanged SCR catalyst materials: correlation of ammonia storage and dielectric properties

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## Abstract

Ammonia-based selective catalytic reduction (SCR) has become the major control strategy for NO<sub>x</sub> emissions from light and heavy duty diesel engines. Before reducing NO<sub>x</sub> on the SCR active material, ammonia storage on the active sites of the catalyst is crucial. The *in operando* measurement of the dielectric properties of the catalyst material using microwave cavity perturbation is a promising indicator of ammonia loading. In this work, results on two zeolite-based SCR materials, i.e. ZSM-5 in H-form and copper ion-exchanged, are presented. The catalyst powder samples were monitored by microwave cavity perturbation as a function of ammonia content at a frequency of approximately 1.2 GHz in a temperature range between 200 and 350 °C. Due to ion exchange, the NH<sub>3</sub> storage behavior changes, what could be monitored in the sensitivity of the dielectric permittivity to NH<sub>3</sub>. In addition, the dependence of the complex dielectric permittivity on ammonia loading is decreased by ion exchange, hinting that mostly ammonia storage on Brønsted sites affects the dielectric permittivity. This finding adds new knowledge to the electrical conduction and polarization mechanisms occurring in these zeolite materials.

## Keywords

NH<sub>3</sub> storage, microwaves, cavity perturbation, zeolites, ZSM-5

## Introduction

One of the continuously challenging factors for automotive manufacturers are the stringent emission standards of nitrogen oxides (NO<sub>x</sub>) for combustion engines and the necessity to develop effective exhaust gas aftertreatment systems to meet the regulations. For leanly operated engines, mostly light and heavy duty diesel engines, in particular, ammonia-based selective catalytic reduction (SCR) has

become the major NO<sub>x</sub> emission control strategy to meet actual and forthcoming emission standards [1]. Today, the focus for SCR-catalysts is on zeolites with active components like iron (Fe) and copper (Cu) [2,3]. In automotive applications, the ammonia-based SCR uses a non-toxic, aqueous urea solution (AdBlue™, DEF) as a reducing agent. The injected solution decomposes by hydrolysis to ammonia (NH<sub>3</sub>) and carbon dioxide (CO<sub>2</sub>) in the hot exhaust. Before the SCR reactions take place, a previous NH<sub>3</sub> adsorption on the acidic sites on the zeolite surface is an essential precondition. This NH<sub>3</sub> storage ability also offers the benefit to buffer changes of flow and temperature in order to ensure a permanent NO<sub>x</sub> conversion. The catalyst reduces NO<sub>x</sub> selectively to nitrogen (N<sub>2</sub>) and water (H<sub>2</sub>O). The two main SCR reactions are shown in the following: the “standard” SCR reaction (Eq. 1) with NO and the “fast” SCR reaction (Eq. 2) with equimolar amounts of NO and NO<sub>2</sub> [4]:



Both, the capacity to store NH<sub>3</sub> and the catalytic activity of zeolite SCR catalysts show a strong dependence on the number and the strength of the acid sites of the zeolite (Lewis and Brønsted sites). Basically, NH<sub>3</sub> adsorption can occur strongly on Brønsted acid sites and weakly as a coordination layer around the strongly bound species via hydrogen bonds or on Lewis sites [5,6]. Due to chemical NH<sub>3</sub> adsorption, the proton conductivity of the zeolite increases distinctly. Due to the different mechanisms, it depends on temperature in a non-Arrhenius manner [5,7]. In order to determine the number of acid sites, temperature-programmed desorption (TPD) of NH<sub>3</sub> is common, but an unambiguous discrimination between Lewis and Brønsted sites is still not possible [8]. Therefore, the approach to correlate dielectric properties under reaction conditions with the catalytic and NH<sub>3</sub> storage behavior *in situ* holds promise for additional information to identify acidic sites or optimize the catalyst material. Here, the cavity perturbation method, which uses microwaves in the GHz range, is suitable, not least because it is non-invasive (apart from interaction with a low power microwave field) and contactless.

Recently, a similar approach closer to automotive on-road applications has been suggested, examining serial-type catalyst devices (as applied in exhaust gas aftertreatment systems with volumes of about 1.5 to 2 liters) [9]. Since the metal canning of the catalyst is used as cavity resonator, the sample occupied most of the cavity volume. Hence, these systems are suitable for real-world applications but not to characterize material properties owing to their very large perturbation of the sample on the cavity space. Already, successfully tested applications include the determination of the oxygen loading of three-way catalytic converters [9-12], or the soot loading [13,14] or ash loading [15] of full-sized diesel particulate filters. The storage degree of NO in lean NO<sub>x</sub> traps [10,16] and the NH<sub>3</sub> loading on SCR catalyst devices have also been successfully monitored [17,18,19] using the cavity perturbation method.

In a previous work, a laboratory test setup for catalyst powder characterization under reaction conditions by microwave cavity perturbation with the ability to determine the dielectric properties of catalyst material *in operando* was developed [20]. It enables the direct measurement of the complex permittivity of catalytic powder samples undergoing gas storage and catalytic reactions in a defined gas atmosphere,

with gas analyzers up- and downstream of the catalyst sample. In the actual, improved version, it operates within a temperature range from room temperature (where usually no reactions occur) to 400 °C.

## Methods

In this work, a microwave cavity perturbation technique operating at approximately 1.2 GHz was applied for material characterization, which uses standing electromagnetic waves (i.e. resonances) inside a defined, hollow cylindrical shaped aluminum cavity. The insertion of a small sample into the cavity resonator leads to a minor perturbation of the electromagnetic field distribution. To determine the dielectric permittivity of the sample, the latter is placed within a region of maximum electric field (and zero magnetic field). For the  $TM_{010}$  mode, which is analyzed in this work, this region is along the entire cylinder axis. The resulting decrease of the resonance frequency and the increase of the 3 dB bandwidth (i.e. decrease of the quality factor  $Q$ ) of the resonance curve are related to real and imaginary parts, respectively, of the complex dielectric permittivity  $\varepsilon = \varepsilon_1 - j\varepsilon_2$  of the sample: the real part  $\varepsilon_1$  (or, more properly,  $\varepsilon_1 - 1$ ) quantifies the polarization of the material and the imaginary part  $\varepsilon_2$  quantifies the dielectric loss. Together with the volume of the sample  $V_s$  and the mode volume of the resonator  $V_{eff}$  (which for the  $TM_{010}$  mode is 26.9% of the enclosed volume of the cylinder), the complex dielectric permittivity can be calculated using equations 3 and 4 [21].

$$\frac{(f_0 - f_s)}{f_0} \approx (\varepsilon_1 - 1) \frac{V_s}{2V_{eff}} \quad (3)$$

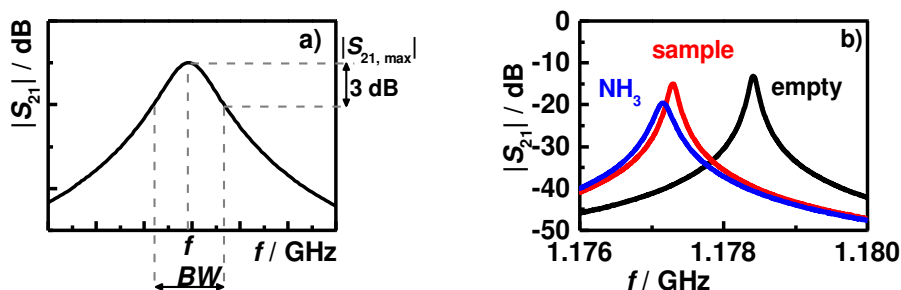
$$\frac{1}{Q_s} - \frac{1}{Q_0} = \Delta \left( \frac{1}{Q} \right) \approx \varepsilon_2 \frac{V_s}{V_{eff}} \quad (4)$$

The resonance peak in the frequency spectrum of the transmission parameter  $S_{21}$ , together with the parameters considered for microwave analysis, are shown in Fig. 1(a), namely: the resonance frequency with sample  $f_s$ , the 3 dB (or “half-power”) bandwidth  $BW$ , and the peak height  $|S_{21,max}|$ . To calculate  $\varepsilon_1$  from Eq. 3, the resonance frequency shift is used and for the calculation of  $\varepsilon_2$  by Eq. 4, the unloaded quality factor  $Q$  is required, from which the effects of cavity coupling have been removed. The used (and in [20] described) cavity is designed (and measured) to have symmetric coupling, i.e. equal inductive coupling strength at each of its two ports, so the coupling unloading process can be calculated using Eq. 5 [21].

$$Q = \frac{f}{BW} \left( 1 - 10^{-|S_{21,max}|/20} \right) \quad (5)$$

where the value of resonant frequency is  $f_0$  for calculation of  $Q_0$  (without the sample), or  $f_s$  for calculation of  $Q_s$  (with the sample). In this work, the microwave parameters were determined by a complex analysis approach using the frequency-phase relation for significantly higher measurement accuracy compared to scalar Lorentzian type curve fitting [22,23].

The microwave parameters were measured using a vector network analyzer (Anritsu Shockline MS46322A). The effects on the transmission signal are displayed in Fig. 1(b). The peak of the empty cavity (black) shifts to a lower frequency and decreases slightly in peak height as the sample is inserted (red). The  $\text{NH}_3$  saturated sample leads to an additional frequency shift and to a stronger decrease in peak height.



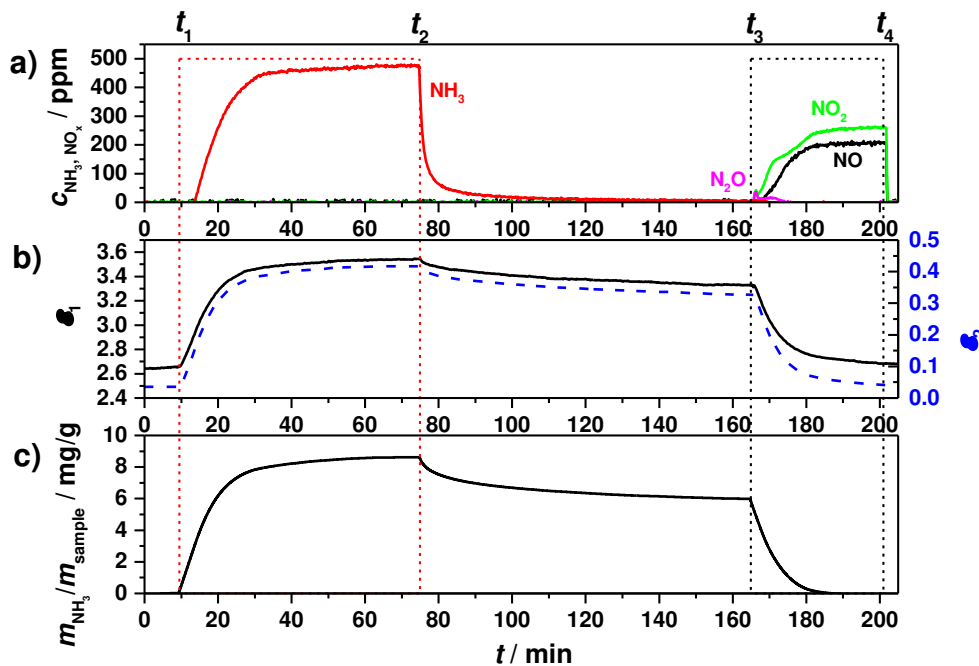
**Figure 1** (a) An exemplary resonance peak in detail, showing the resonant frequency  $f$ , 3 dB bandwidth  $BW$ , and maximum peak height  $|S_{21, \text{max}}|$ , (b) resonance peaks at 200 °C of the empty sample tube (black), with inserted H-ZSM-5 sample (red), and with the H-ZSM-5 sample loaded with  $\text{NH}_3$  (blue)

The zeolite under test was a H-ZSM-5 powder with a Si/Al ratio of 27 (Clariant International Ltd.). The Cu-ZSM-5 was prepared by aqueous ion-exchange of the H-ZSM-5. The Cu ion-exchange level was determined to an atomic ratio of Cu:Al of 0.11 by EDX. Both samples were weighted and their skeletal volumes were determined using a helium gas pycnometer. All measurements were performed on a test bench setup described in [20] with a total gas flow of 1 l/min and a background gas composition of 2 %  $\text{H}_2\text{O}$  balanced with  $\text{N}_2$ . All gas flows were controlled by mass flow controllers (MFCs, MKS) and the downstream gas concentrations were monitored by a Fourier Transformed Infrared Spectroscopy (FTIR) analyzer (Nicolet Antaris IGS).

## Results and Discussion

Figure 2 shows a storage measurement on H-ZSM-5 at 200 °C. In Fig. 2(a), the inlet (MFC data, dashed) and outlet (FTIR data, solid) gas concentrations of  $\text{NH}_3$ , NO,  $\text{NO}_2$  and  $\text{N}_2\text{O}$  are shown. From these data, the adsorbed amount of  $\text{NH}_3$  on the zeolite is calculated and is shown in mg per gram of sample in Fig. 2(c). In Fig. 2(b), the measured real and imaginary parts of the permittivity are presented. After 10 minutes in background gas (at  $t_1$ ), 500 ppm  $\text{NH}_3$  were fed and immediately, both parts of the permittivity are seen to increase due to the adsorption of  $\text{NH}_3$ . Initially, the zeolite stores all of the incoming  $\text{NH}_3$ , indicated by the fact that no  $\text{NH}_3$  can be detected downstream by the FTIR analyzer. After 65 minutes (at  $t_2$ ), the  $\text{NH}_3$  concentration downstream almost reached the inlet concentration and the permittivity values remained at a constant level, indicating that the catalyst was saturated with  $\text{NH}_3$ . Thus,  $\text{NH}_3$  was turned off and the weakly bound  $\text{NH}_3$  was desorbed or released during the following 90 minutes, seen in a slow decrease in the downstream concentration of  $\text{NH}_3$  and the permittivity. When no  $\text{NH}_3$  was detected downstream anymore (at  $t_3$ ), 10 %  $\text{O}_2$ , 250 ppm NO and 250 ppm  $\text{NO}_2$  were admixed to convert

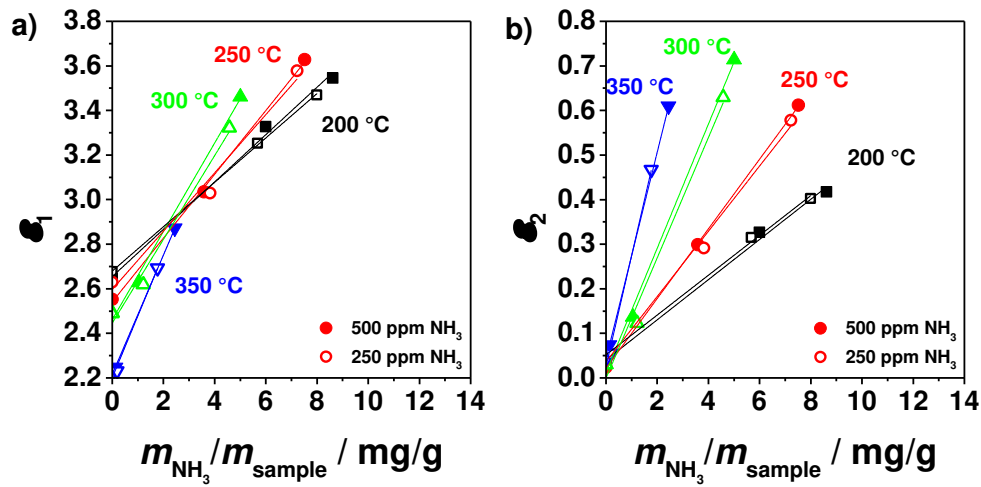
the remaining strongly bonded  $\text{NH}_3$  according to the “fast” SCR reaction (Eq. 2), until the zeolite was free of  $\text{NH}_3$  (at  $t_4$ ) as the overall  $\text{NO}_x$  concentration downstream reached the inlet concentration and the permittivity returned to its values of the beginning of the measurement. One clearly can see the good correlation between the stored amount and the measured complex permittivity.



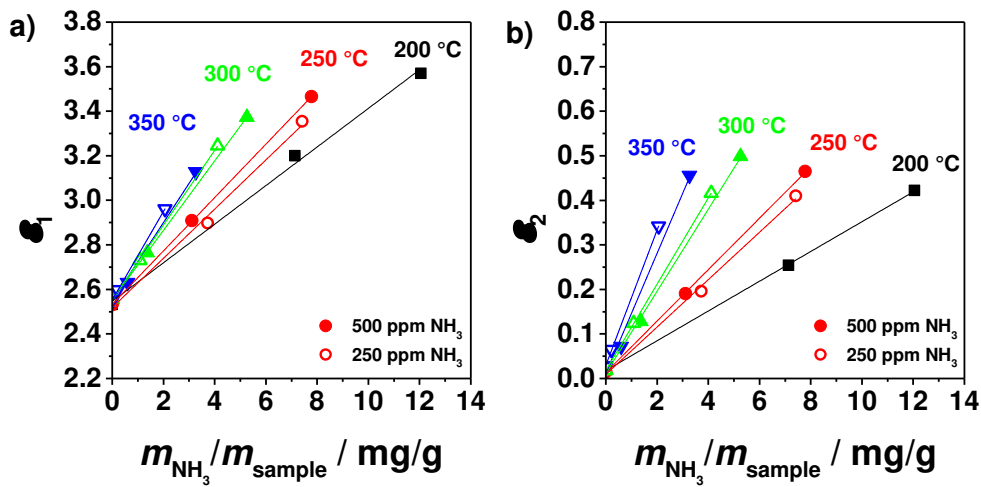
**Figure 2** Storage measurement on H-ZSM-5 at 200 °C. (a) Inlet (dashed) and outlet (solid) gas concentrations of  $\text{NH}_3$  (red),  $\text{NO}$  (black) and  $\text{NO}_2$  (green) and  $\text{N}_2\text{O}$  (magenta), (b) real (black) and imaginary (blue, dashed) part of the permittivity and (c) calculated amount of  $\text{NH}_3$  adsorbed on the catalyst

The same experiment as shown in Fig. 2 was performed at temperatures of 200, 250 300 and 350 °C on the H-form and the Cu exchanged ZSM-5 sample with inlet concentrations of  $\text{NH}_3$  of 250 and 500 ppm. For the subsequent analysis, three steady states were evaluated for each measurement: the  $\text{NH}_3$  free condition at the beginning of the measurement, the saturated state (at  $t_2$ ), where the total stored amount was determined, and the point when the free desorption was finished (at  $t_3$ ), where the strongly bound fraction was identified. In Fig. 3,  $\epsilon_1$  and  $\epsilon_2$  are plotted at the three mentioned states over the adsorbed amount on the H-ZSM-5 powder. Measurements with an  $\text{NH}_3$  inlet concentration of 250 ppm (open symbols) and 500 ppm (filled) are shown at different temperatures. One can see, especially in the plot of  $\epsilon_2$ , that the total stored amount of  $\text{NH}_3$  reduces with increasing temperature from 8.6 mg per g powder sample at 200 °C to 2.4 mg/g at 350 °C for an inlet concentration of 500 ppm. Furthermore, it is apparent that the total adsorbed amount is dependent on the partial pressure of  $\text{NH}_3$ , as the total stored amount for the inlet concentration of 250 ppm is lower than for 500 ppm, especially at the higher temperatures, where  $\text{NH}_3$  is mainly weakly bound. The strongly bound fraction of  $\text{NH}_3$  is only dependent on the number of Brønsted acid sites, which can be seen by the almost identical values of strongly bound  $\text{NH}_3$  for 250 and 500 ppm.  $\epsilon_1$  without ammonia has values between 2.2 and 2.7, but is decreasing with temperature. For all temperatures,  $\epsilon_1$  increases linearly with the stored mass of  $\text{NH}_3$ , with a slope

slightly increasing with temperature.  $\epsilon_2$  is almost zero in the unloaded state at each temperature, as the zeolite is an almost lossless material. The dielectric losses increase linearly with stored  $\text{NH}_3$  and show a higher dependency on temperature compared to  $\epsilon_1$ , as the slopes increase more strongly with increasing temperature.



**Figure 3** (a)  $\epsilon_1$  and (b)  $\epsilon_2$  as a function of stored amount of  $\text{NH}_3$  for H-ZSM-5 at 200 °C (black), 250 °C (red), 300 °C (green) and 350 °C (blue) for measurements with 250 ppm (open symbols) and 500 ppm (filled) inlet concentration of  $\text{NH}_3$



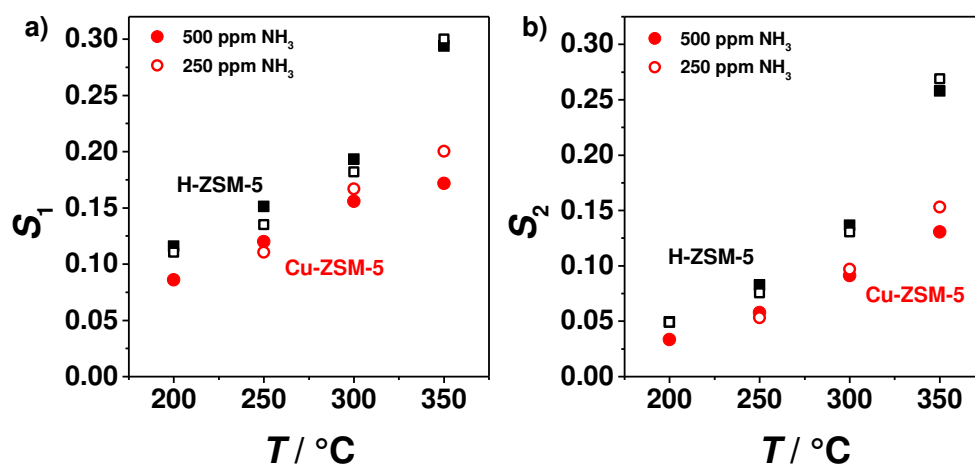
**Figure 4** (a)  $\epsilon_1$  and (b)  $\epsilon_2$  over stored amount of  $\text{NH}_3$  for Cu-ZSM-5 at 200 °C (black), 250 °C (red), 300 °C (green) and 350 °C (blue) for measurements with 250 ppm (open symbols) and 500 ppm (filled) inlet concentration of  $\text{NH}_3$

In Fig. 4, the same measurements are shown on the Cu exchanged samples, except for the missing data at 200 °C with 250 ppm inlet concentration. The total stored amount of  $\text{NH}_3$  at 200 °C is higher for this sample compared to the H-form, what is caused by the weak storage on the Cu ions, which can be coordinated by up to four  $\text{NH}_3$  molecules [24]. At higher temperatures, the  $\text{NH}_3$  storage is on the same level as the storage on the H-form. Again, one can see the dependencies on temperature and  $\text{NH}_3$  partial pressure of the total stored amount. The unloaded  $\epsilon_1$  takes similar values to the H-form sample



between 2.5 and 2.6, showing no strong temperature dependence in the unloaded state compared to the H-form. The basic behavior of the slopes for  $\epsilon_1$  appear comparable for both samples.  $\epsilon_2$  shows again a higher temperature dependency than  $\epsilon_1$ , but the overall dielectric losses are smaller than for the H-form. A possible reason therefore is that the losses are predominantly caused by this adsorbed  $\text{NH}_3$ , which is strongly bound to the Brønsted acid sites.

For a better comparison of the two materials, the changes of  $\epsilon_1$  and  $\epsilon_2$  between unloaded and saturated state referred to the total stored amount of  $\text{NH}_3$ , hereafter called sensitivity  $S = \Delta\epsilon/(m_{\text{NH}_3}/m_{\text{sample}})$ , were calculated and are shown in Fig. 5.  $S_1$  (a) and  $S_2$  (b) increase with temperature, which is caused by the thermal activation of the  $\text{NH}_4^+$  ions, as they become more mobile at higher temperatures. The sensitivities of both permittivity values are higher for the H-form, compared to the Cu-ZSM-5. An explanation therefore could be that the  $\text{NH}_3$  species which are coordinatively bound to the copper sites do not influence the permittivity to a large extent. The values for loading with 250 and 500 ppm  $\text{NH}_3$  are nearly similar at each temperature, so that the change of the permittivity is only dependent on the stored amount of  $\text{NH}_3$ .



**Figure 5** Sensitivities of (a)  $\epsilon_1$  and (b)  $\epsilon_2$  for H-ZSM-5 (black) and Cu-ZSM-5 (red) for  $\text{NH}_3$  inlet concentrations of 250 ppm (open symbols) and 500 ppm (filled)

## Conclusion and Outlook

In this study, initial measurements with a recently introduced measurement setup using microwave cavity perturbation for catalyst powder samples were performed on ZSM-5 zeolites in H-form and Cu exchanged. The selected temperature range was 200 °C to 350 °C and all measurements were performed with 2 % water. For both samples, the amount of stored  $\text{NH}_3$  was mirrored by both the real  $\epsilon_1$  and the imaginary parts  $\epsilon_2$  of the complex dielectric permittivity. In storage, both samples behave similarly, the only exception being the Cu exchanged zeolite at 200 °C, which shows significantly higher storage. This might be related to the coordinative binding of  $\text{NH}_3$  to Cu ions at lower temperatures. The H-form shows continuously higher sensitivities of the complex dielectric permittivity to  $\text{NH}_3$  compared to the Cu exchanged sample. A possible explanation is that storage on Cu ions might have only a weak



effect on the measurable dielectric properties compared to storage on Brønsted sites. However, this experimental finding requires further investigations.

In future work, samples with other exchanged ions like iron (Fe) and varying exchange levels will be investigated. Another focus is to perform temperature-programmed desorption experiments. Additionally, frequency dependent measurements of the complex permittivity by analyzing several cavity modes (from 1.1 GHz to 4.2 GHz) are planned.

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